



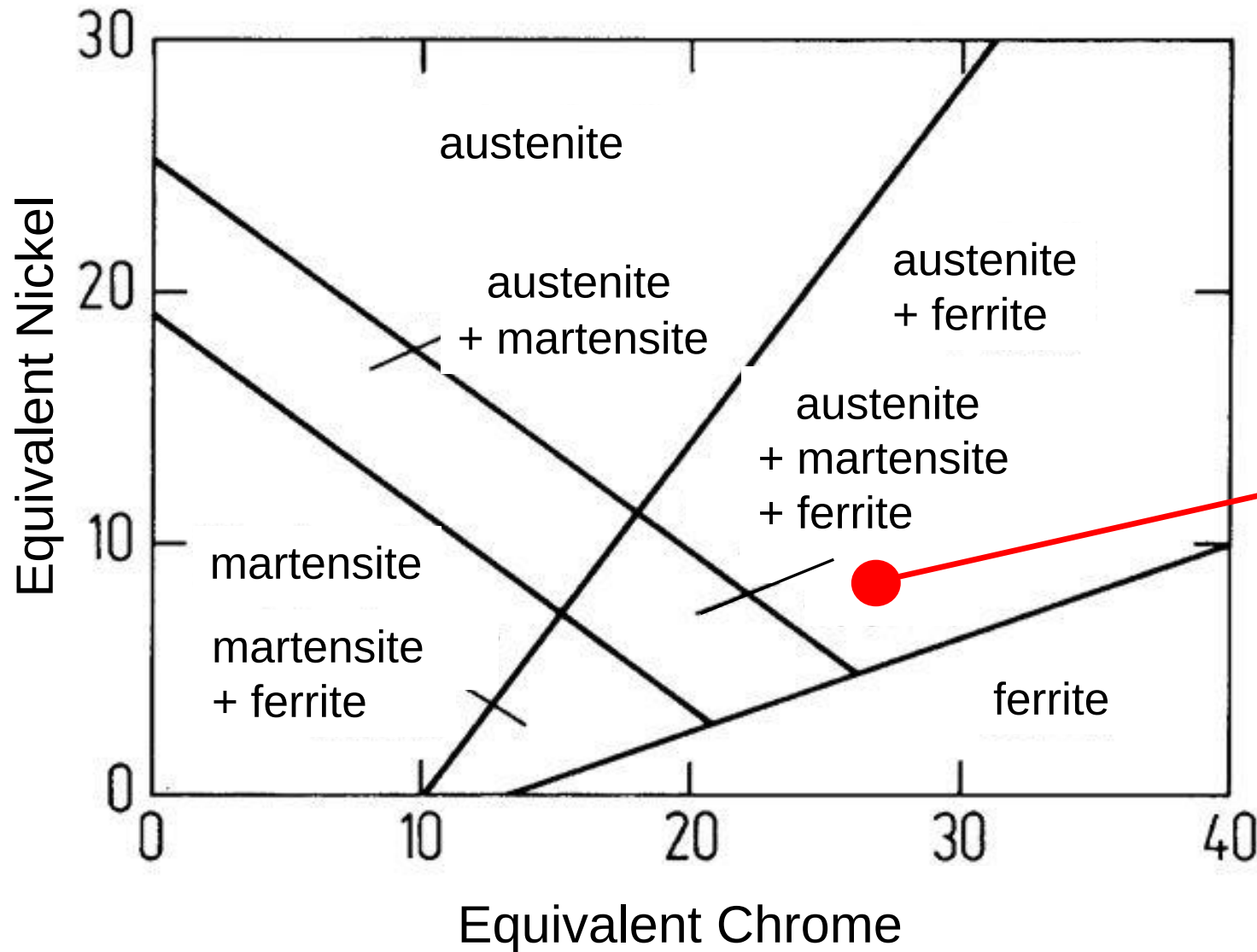
Toughness of duplex steel produced by PM-HIP

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1. Introduction
2. Duplex steel produced by Powder-HIP
3. Influences on impact toughness by
 - production method (as cast, as forged, PM-HIP)
 - local stress triaxiality (notches)
 - sigma phase
 - argon content
4. Summary



Duplex steel:

2205

ASTM F51

AISI 318LN

DIN 1.4462

X2CrNiMoN22-5-3



steel: AISI 318LN

produced by: powder HIP

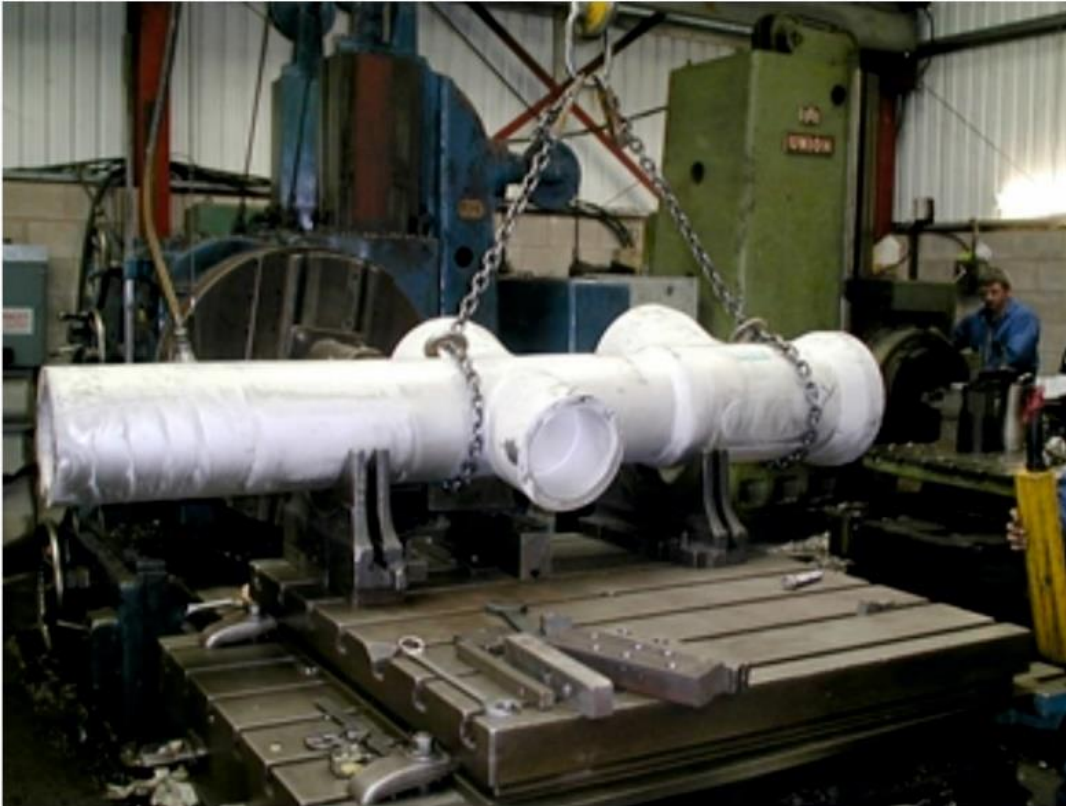
weight: 500 kg

Charpy-V-notch-toughness:

$T = -46^{\circ}\text{C} : a_K = 75 - 110 \text{ J}$

courtesy by: Sandvik Powdermet AB

Collecting pipe for offshore platform “Heidrun”



steel grade: AISI 318LN

production: powder HIP

Charpy-V-notch toughness:

$T = 20^{\circ}\text{C} : a_K > 150 \text{ J}$

$T = -46^{\circ}\text{C} : a_K > 70 \text{ J}$

courtesy by: Metso AB

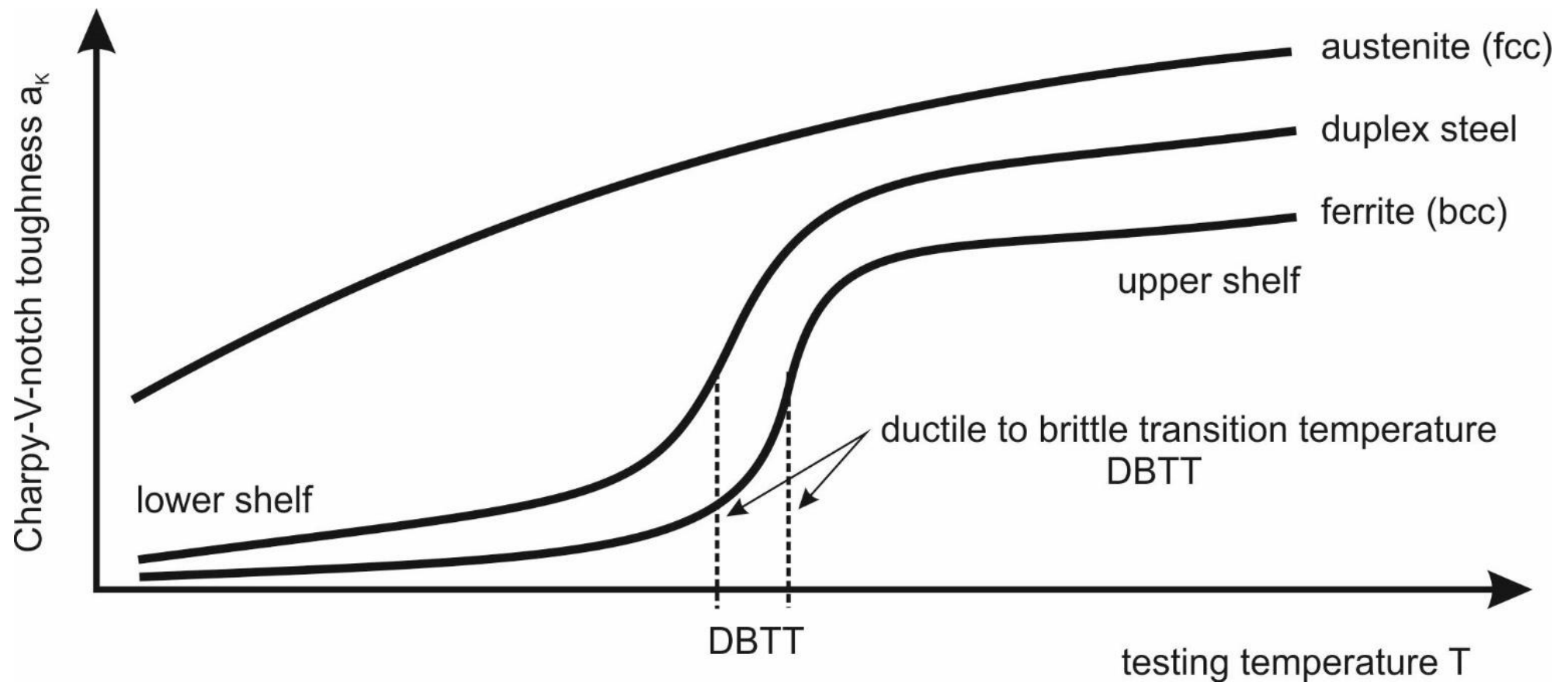
loading conditions:

- thermal activation of deformation mechanisms
 - temperature
 - deformation rate
- stress triaxiality
 - notches

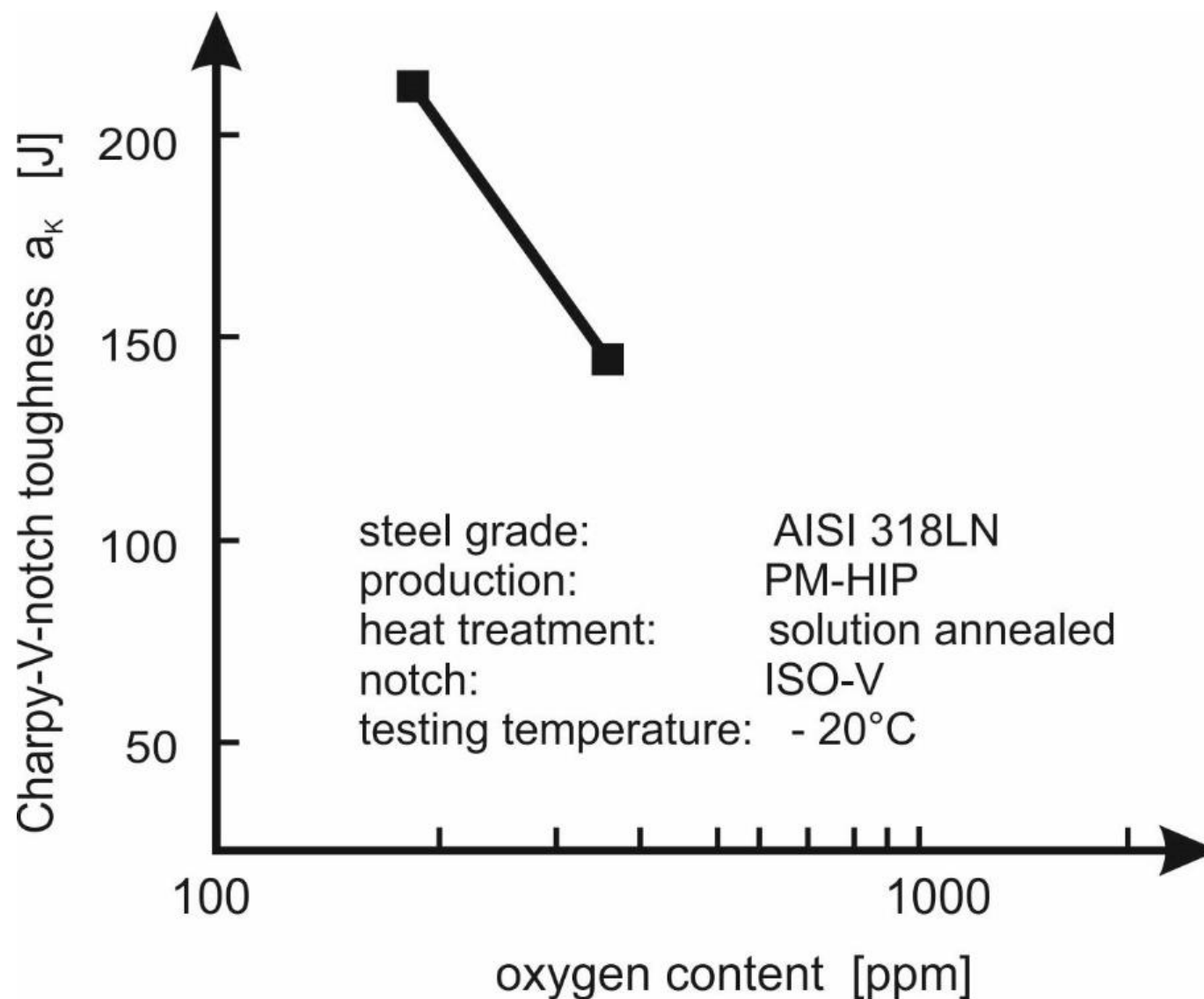
microstructure of the material:

- crystal lattice
- grain size
- non metallic inclusions
- in case of duplex steels: intermetallic phases
 - σ -phase
 - α' -Phase
- in PM-HIP materials
 - oxides at the prior particle boundaries (PPB's)
 - Ar-voids

Toughness – temperature diagram (schematic)



Influence of the oxygen content on the Charpy-V-notch toughness



Chemical composition of the investigated steel grades



production route	chemical composition [weight- %]						
	C	Si	Mn	Cr	Mo	Ni	N
PM HIP (powder)	0,015	0,68	1,02	22,20	3,09	5,19	0,189
continuous cast +	0,020	0,50	1,71	22,46	3,36	5,40	0,184
hot forged							
sand cast	0,029	0,72	1,35	23,07	2,78	6,50	0,181
EN 10088	≤ 0,03	≤ 1,0	≤ 2,0	21,0 - 23,0	2,5 -3,5	4,5 - 6,5	0,10 - 0,22

gas atomized powder:

particle size distribution:

particle size [μm]	500	250	125	106	63	45
fraction < [%]	100	84	47	37	18	10

oxygen content of the powder:

85 ppm

apparent density:

4,69 g/cm³

tap density:

5,30 g/cm³

capsule size:

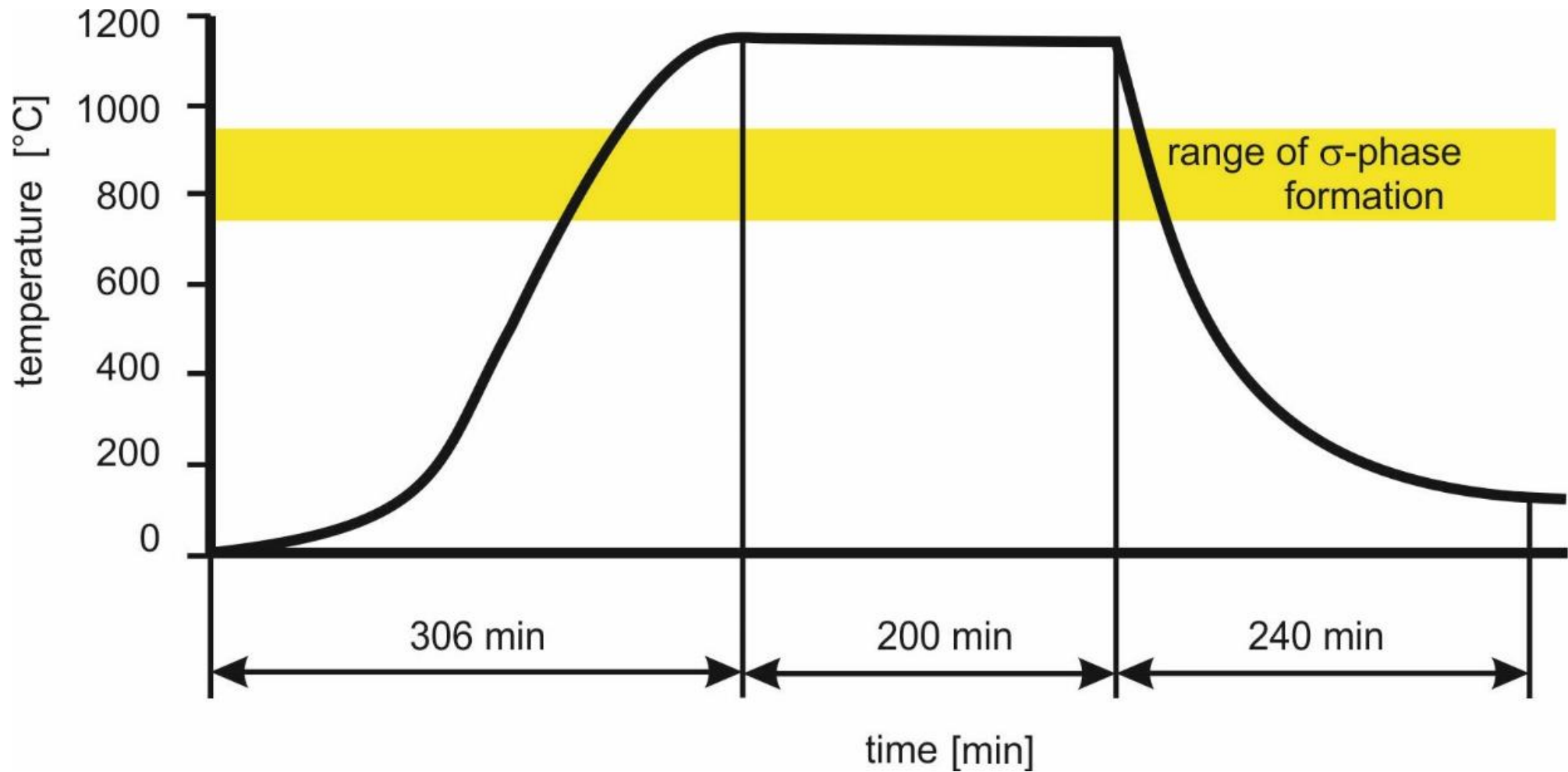
D = 110 / 200 mm, H = 235 mm

HIP-cycle:

holding temperature: 1140 °C

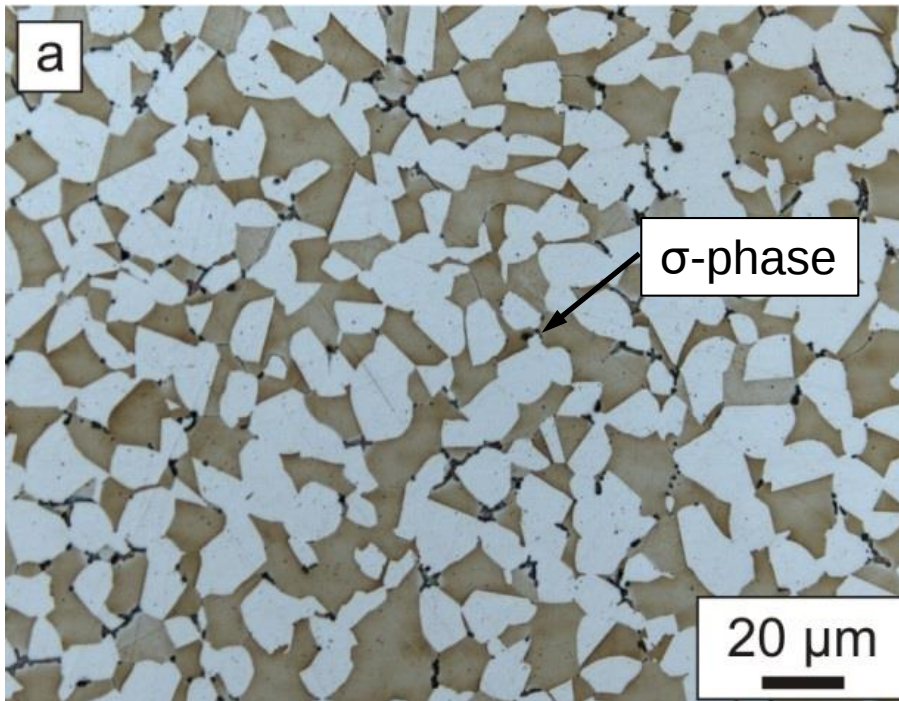
holding time: 200 min

pressure: 1010 bar



time between 940°C and 750°C: 45 min

microstructure as HIP

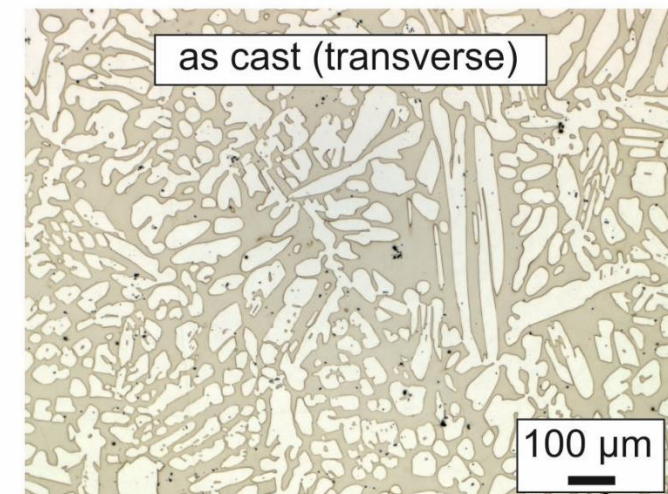
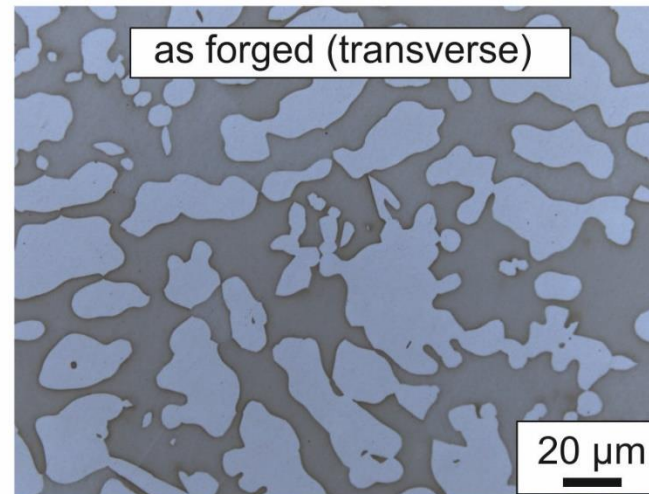
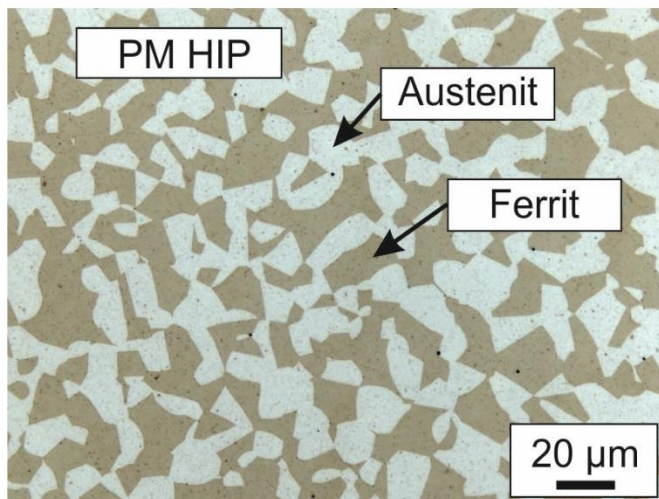
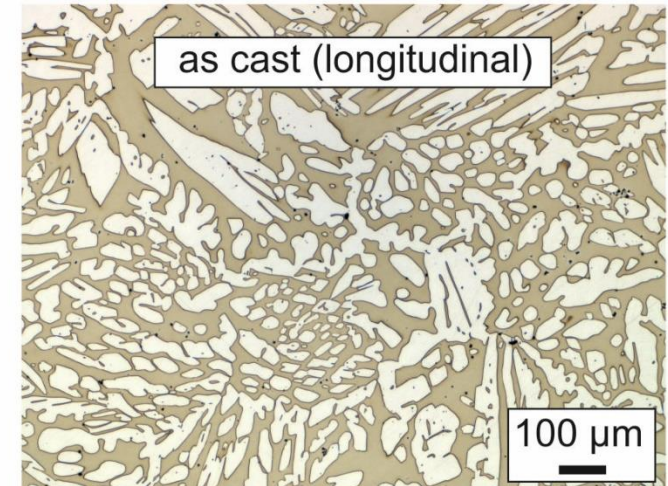
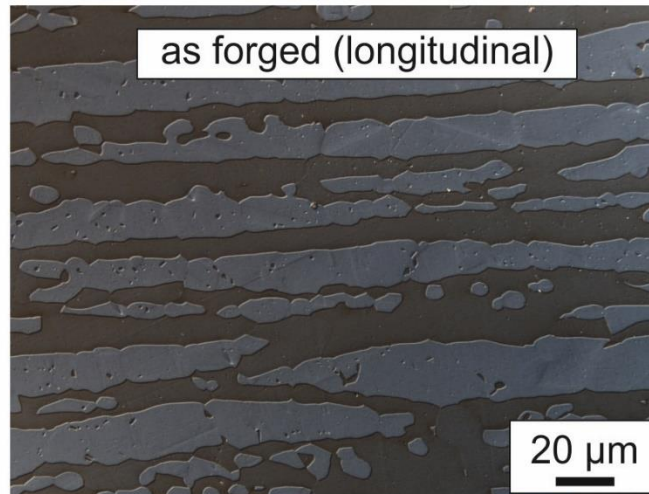
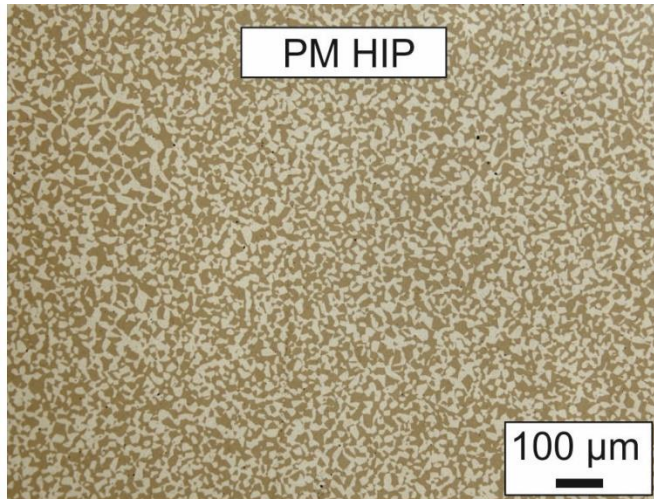


heat treatment of the PM-HIP-grade:

- solution annealing at 1060 °C for 3 h
- quenching in water

State	phase fraction [vol.- %]		
	austenite	ferrite	σ -phase
as HIP	$50,9 \pm 1,3$	$46,8 \pm 2,2$	$1,3 \pm 0,2$
HIP + solution annealed	$50,5 \pm 1,4$	$49,4 \pm 1,4$	0

Microstructure of duplex steel after solution annealing



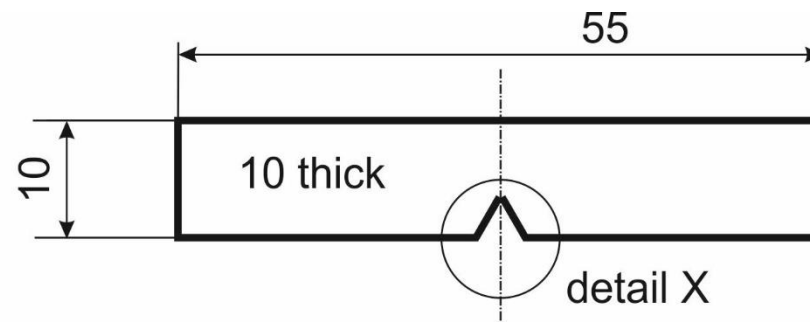
max. energy of the hammer:

300 J

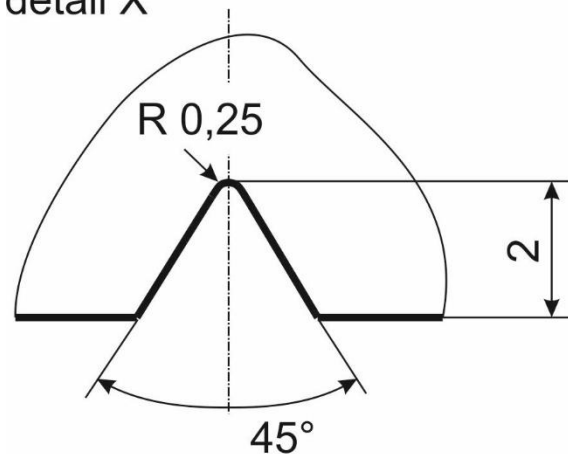
variation of testing temperature:

-196°C bis +400°C

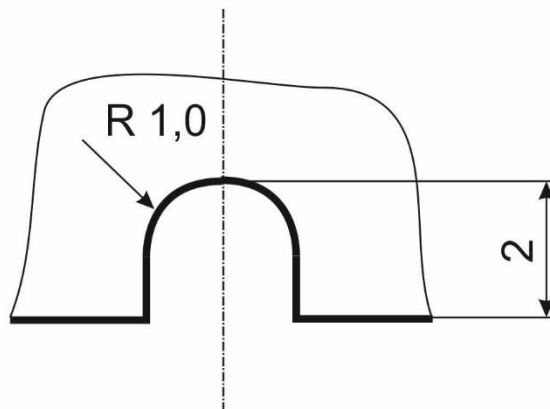
specimen geometry and variation of notch geometry:



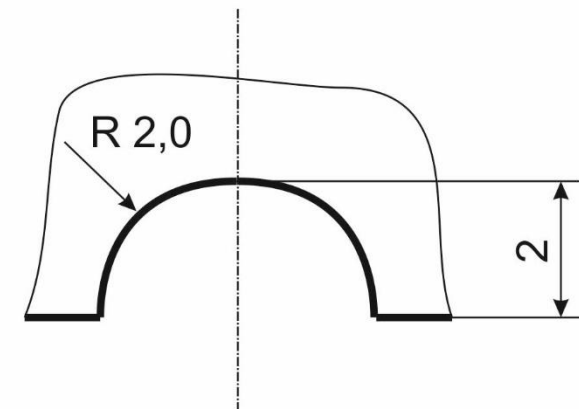
detail X



ISO-V-notch

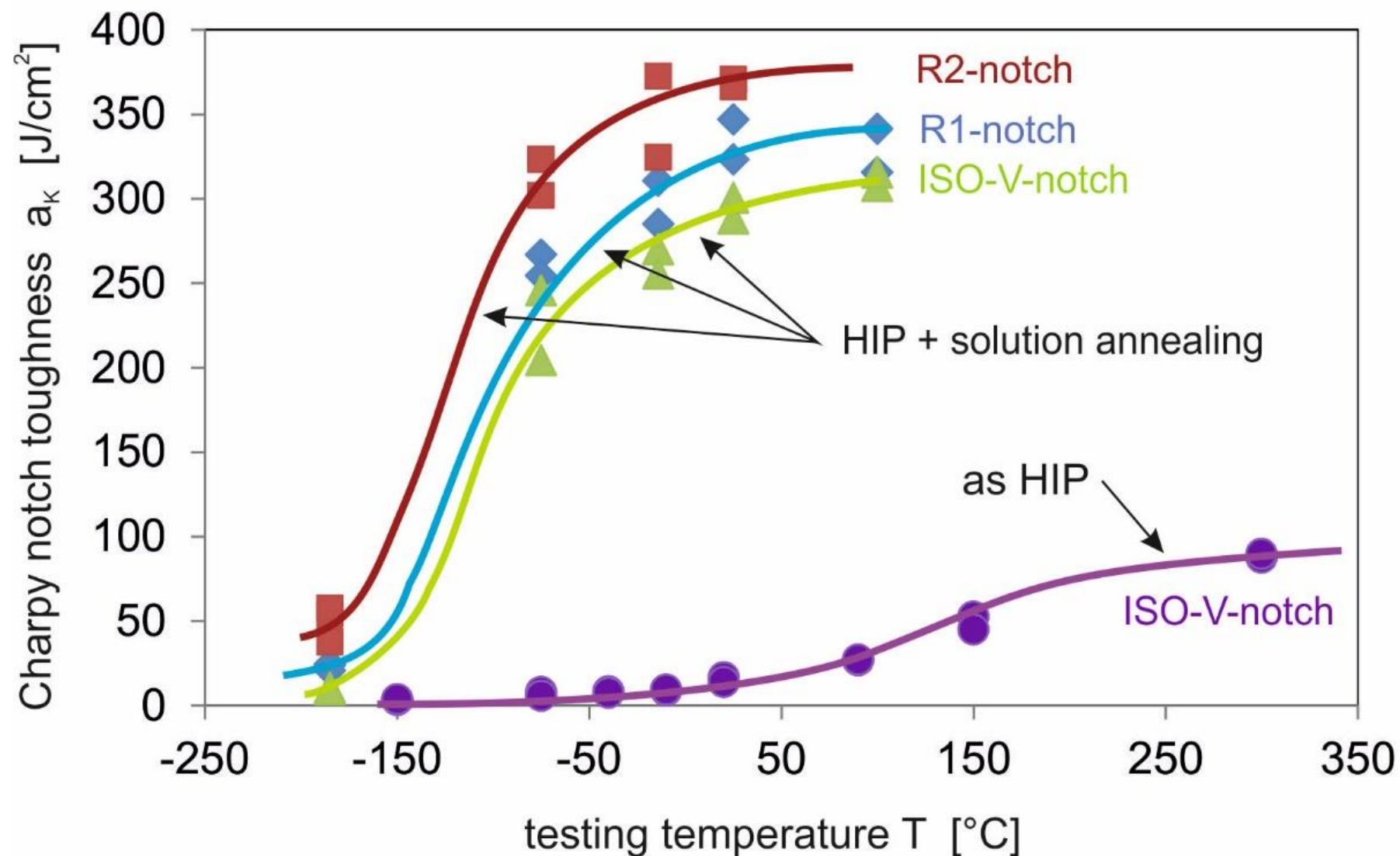


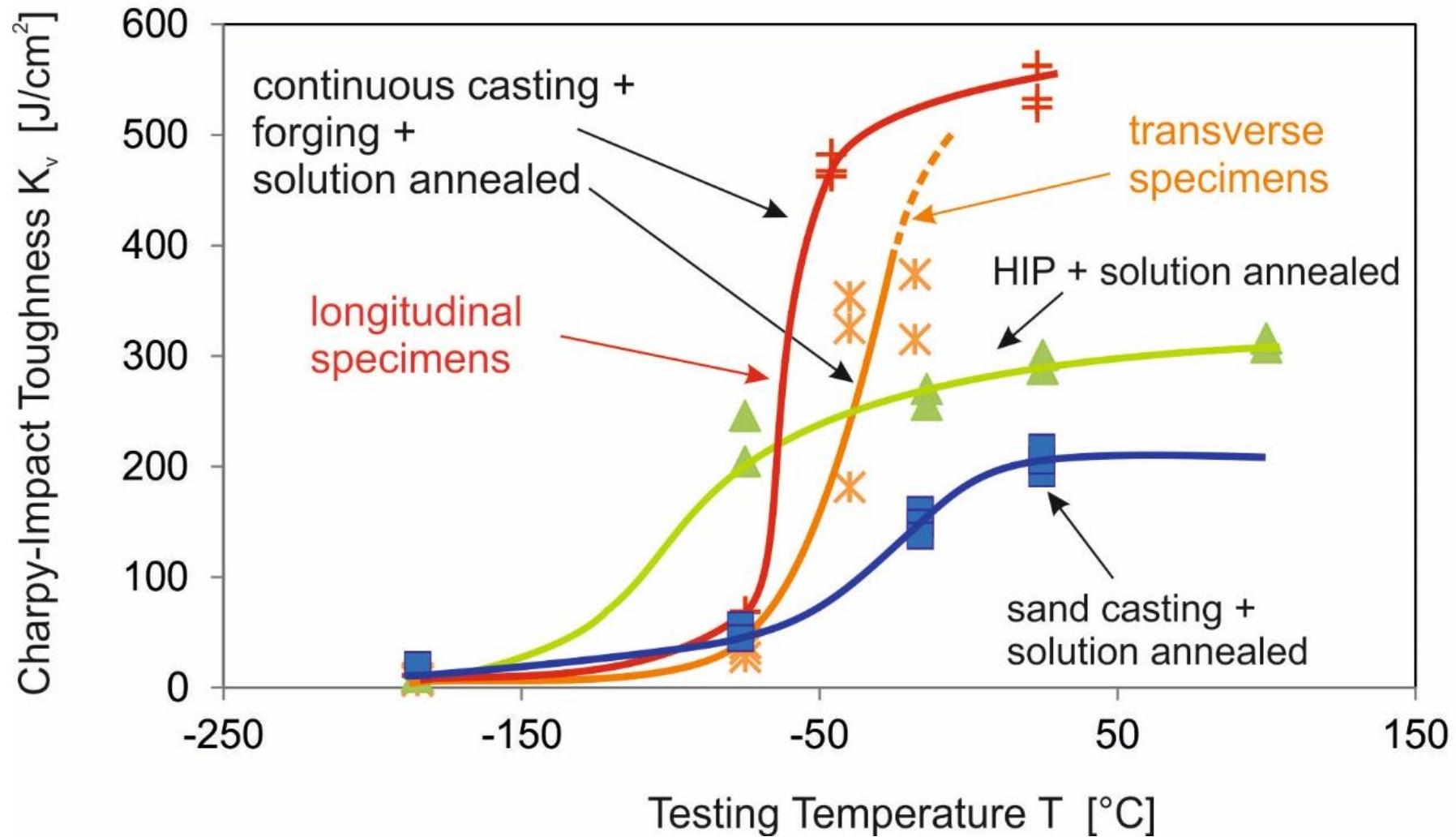
R1-notch



R2-notch

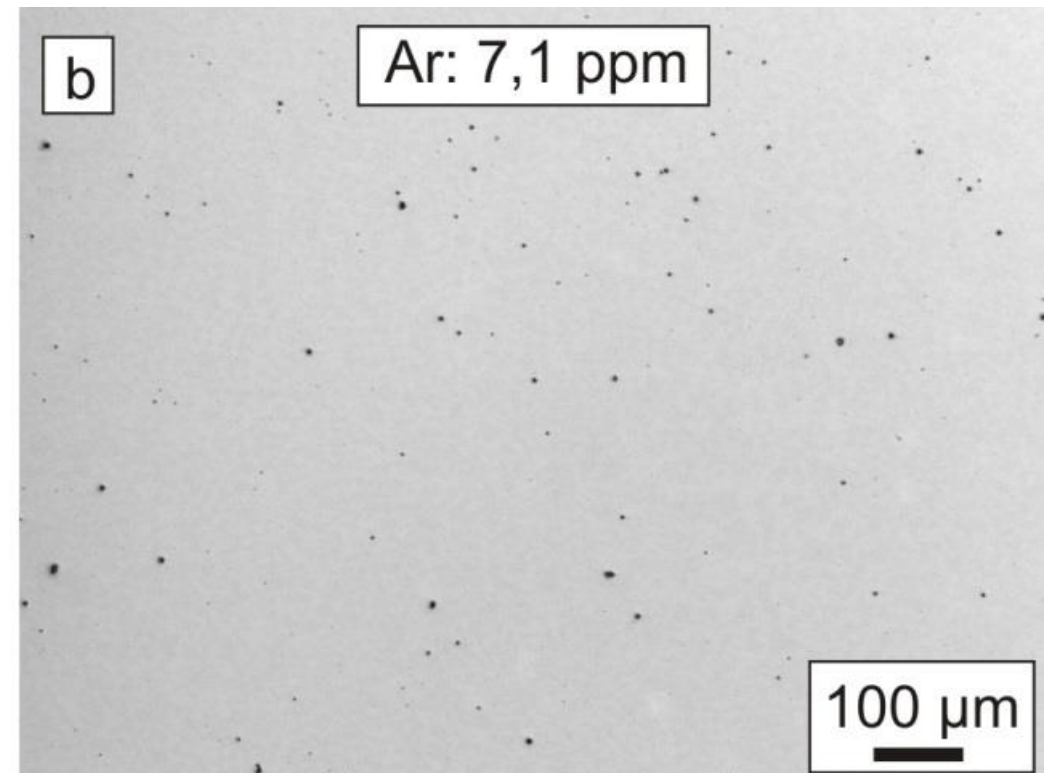
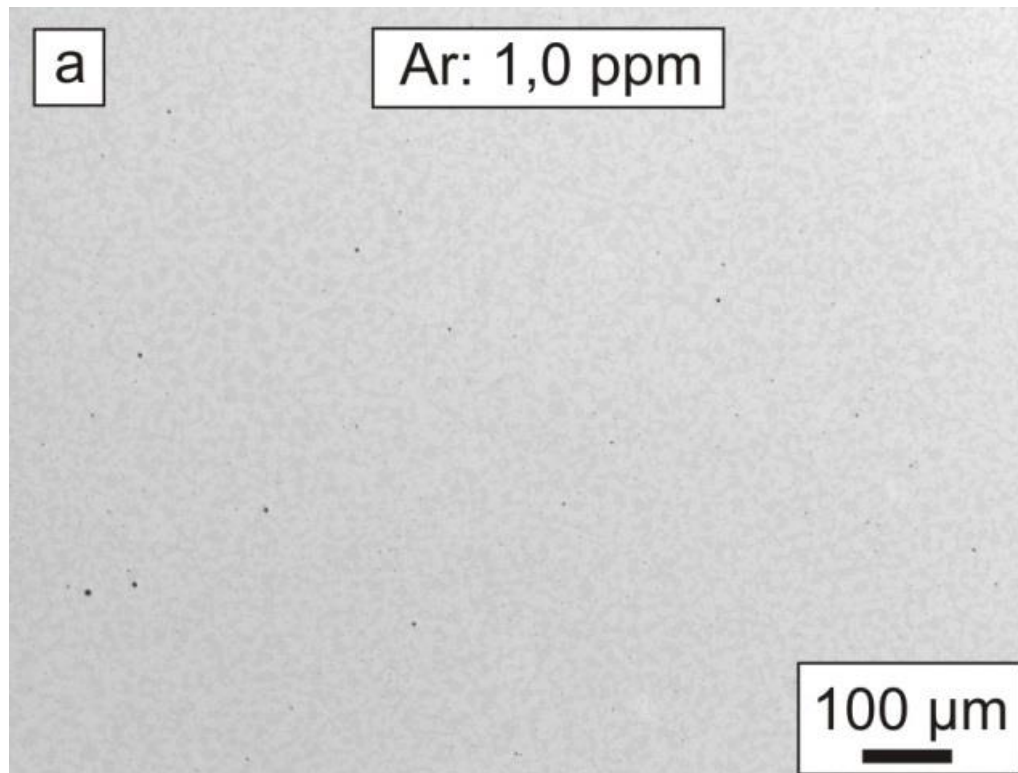
Charpy toughness of PM-HIP duplex steel - influence of heat treatment and notch geometry



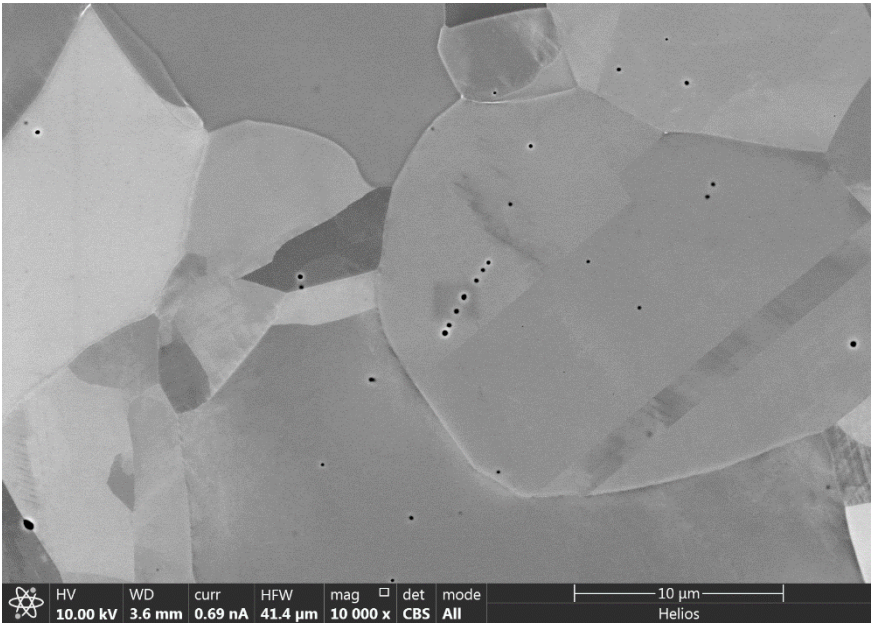
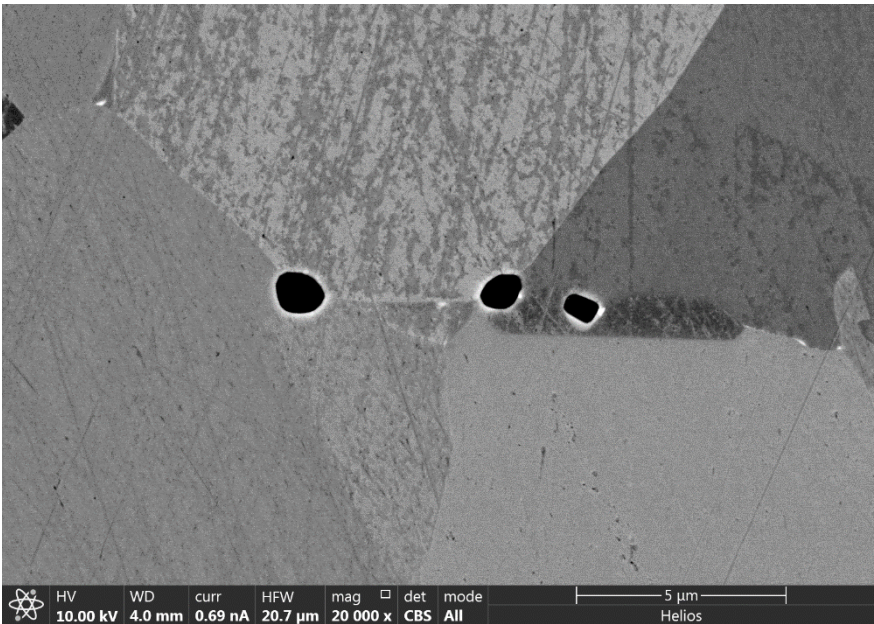
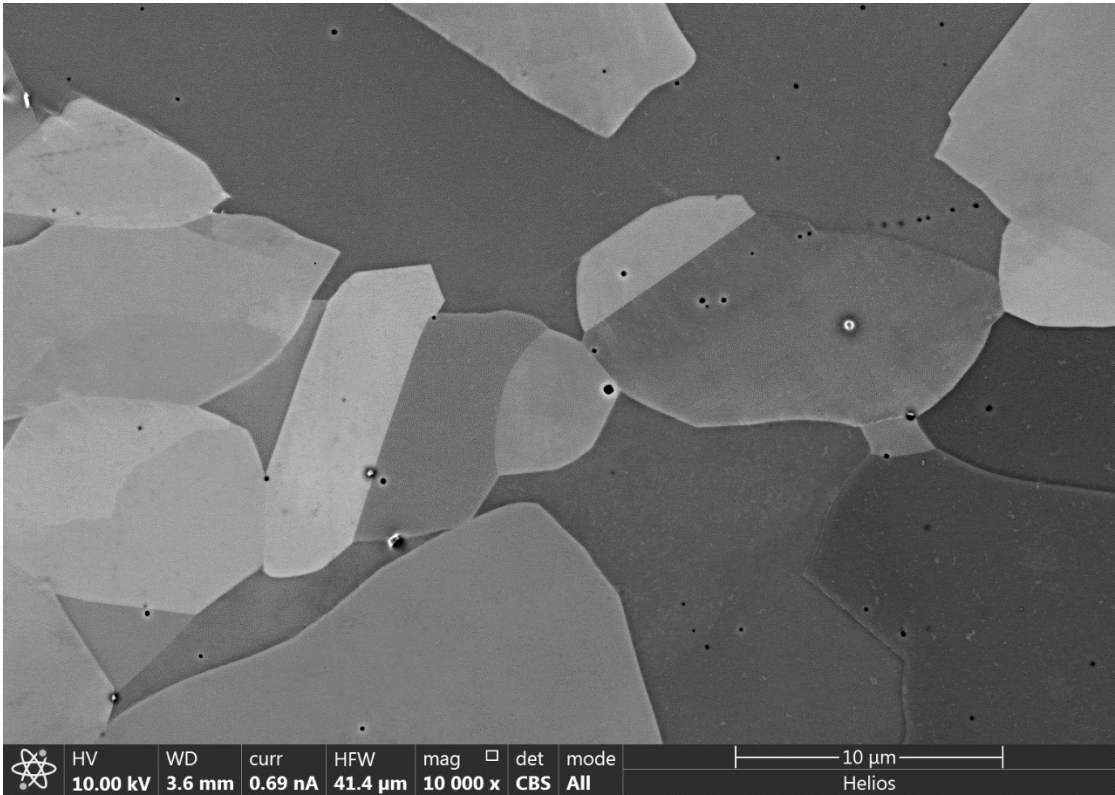


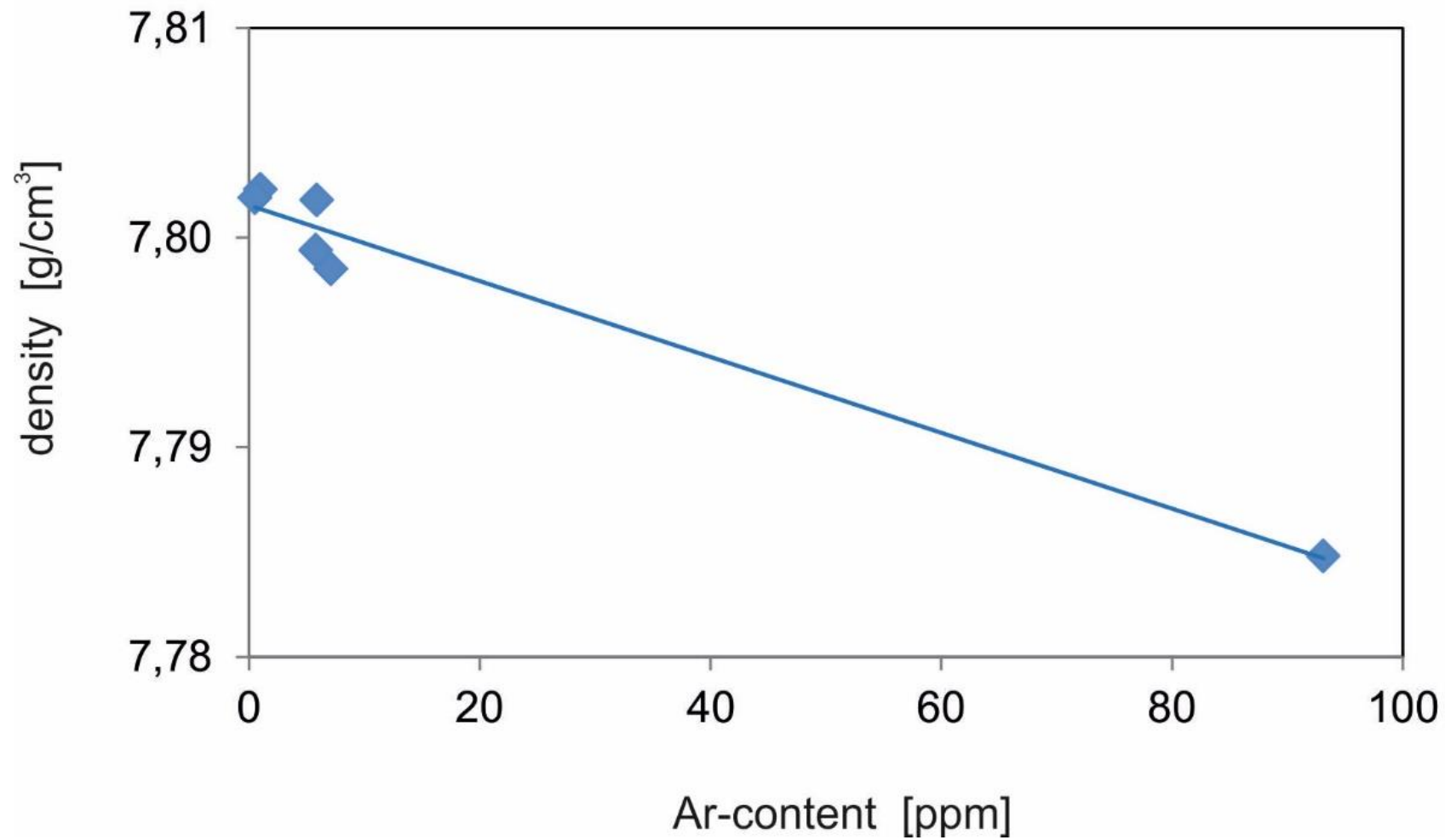
- capsule size: D 110 mm x H 230 mm:
- capsule material: AISI 304
- relative filling density: 66 – 69 %
- evacuation-process:
 - flushing with He for leak test
 - 5 x evacuation down to 10⁻³ mbar and flushing with Ar (1.5 bar)
 - adjusting the final Ar pressure according to the desired Ar-content
- HIP-cycle:

holding temperature:	1140 °C
holding time:	200 min
pressure:	1010 bar
- determination of Ar-content: analyser type Eltra-Werf

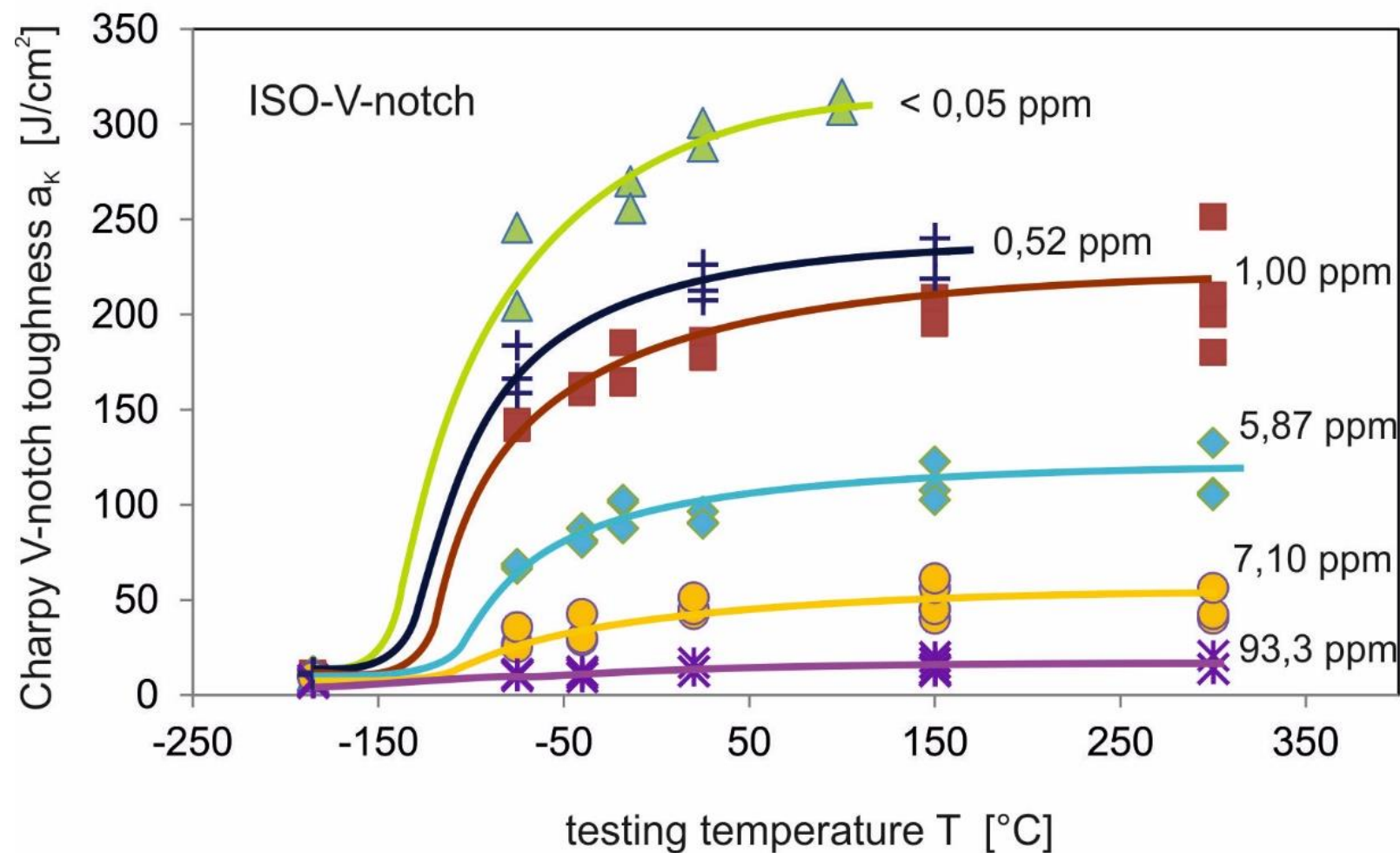


Microstructure with Argon pores in a sample with 1.0 ppm Ar

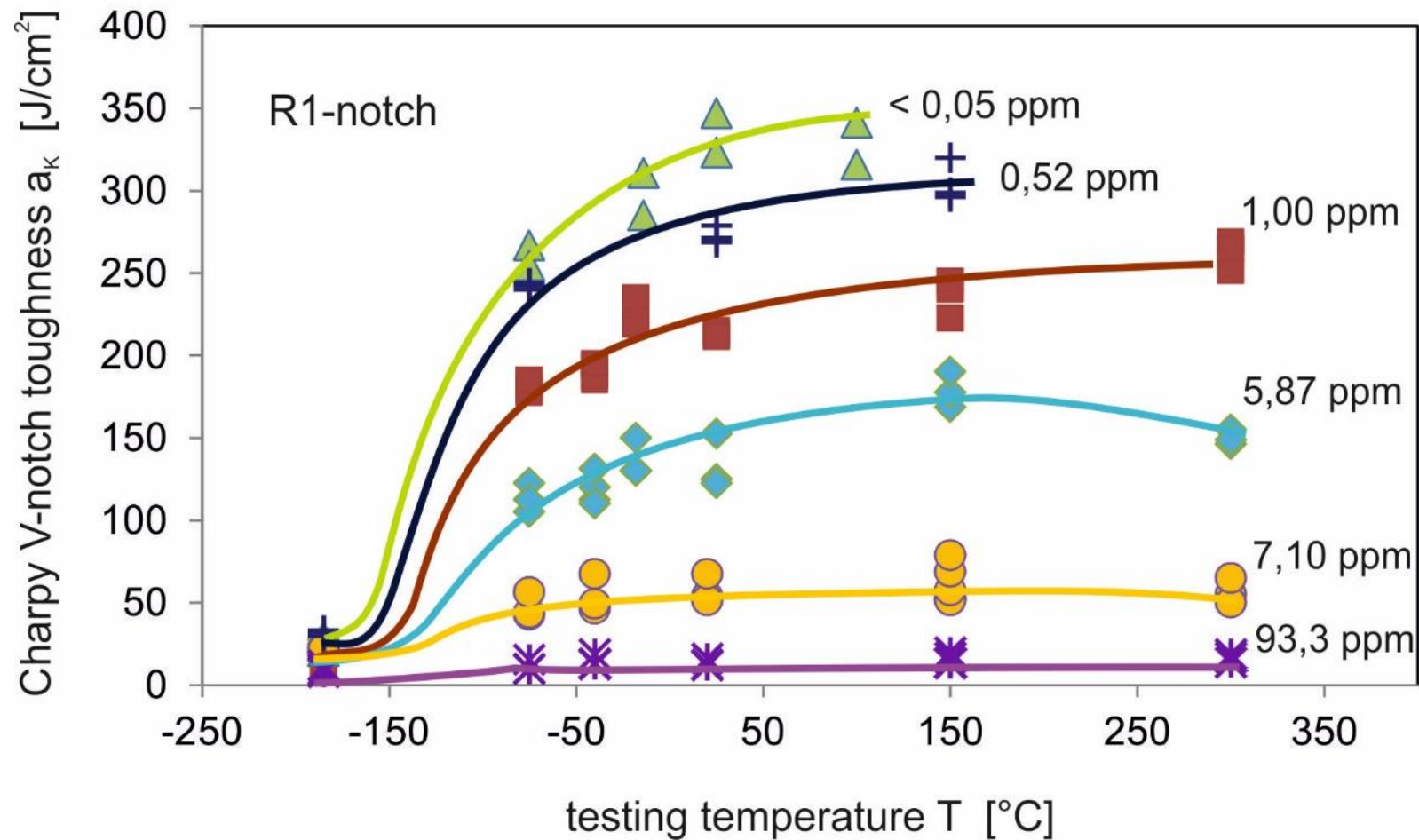




Influence of Argon content on notch toughness – V-notch

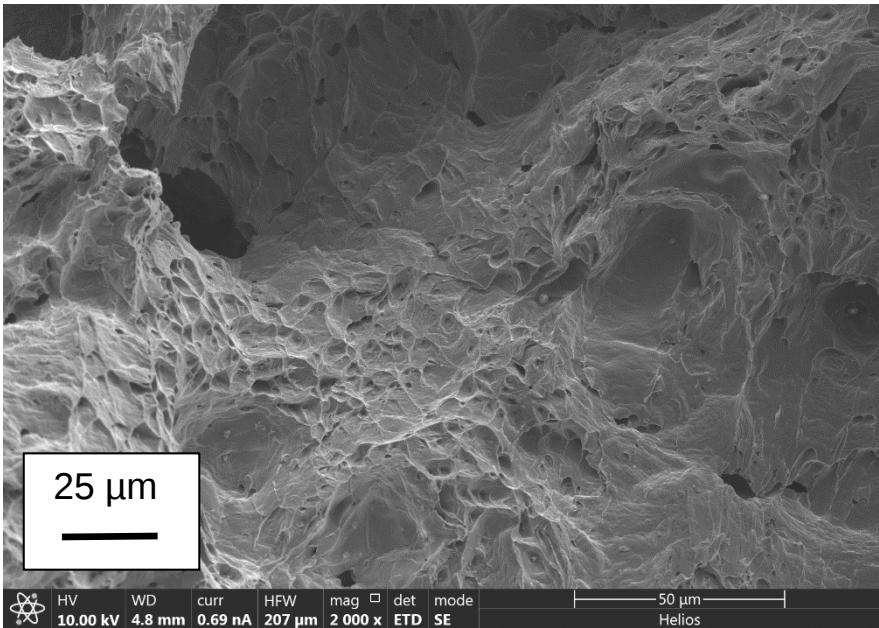
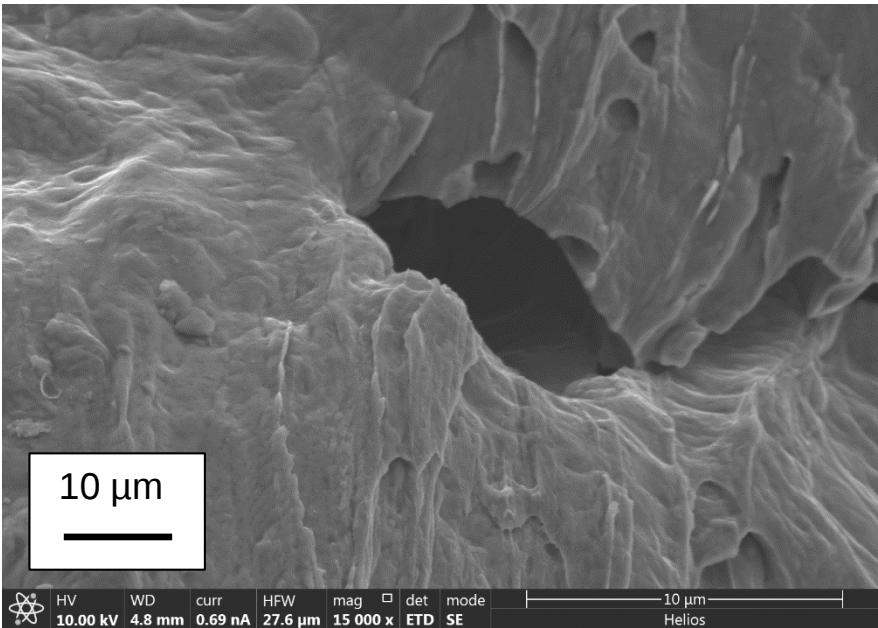
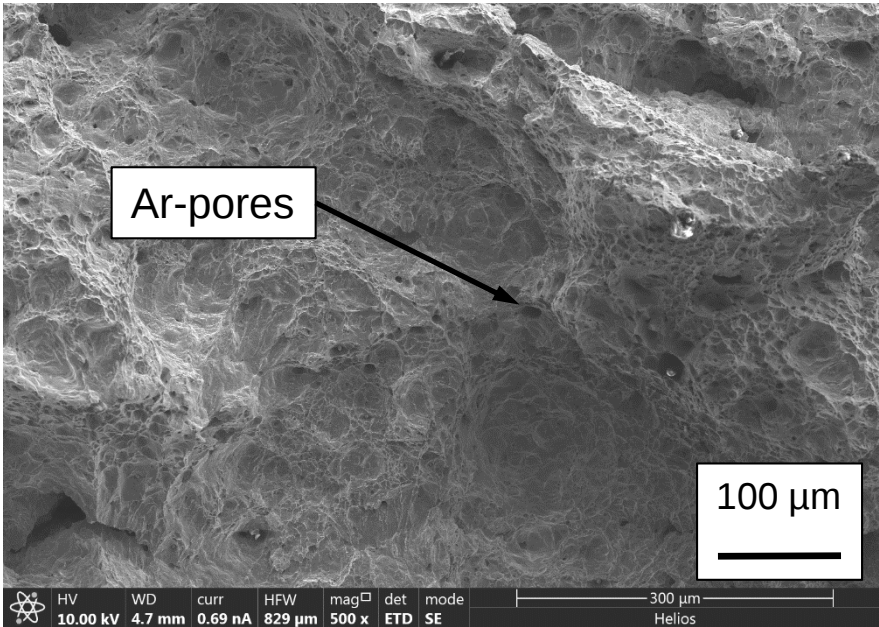
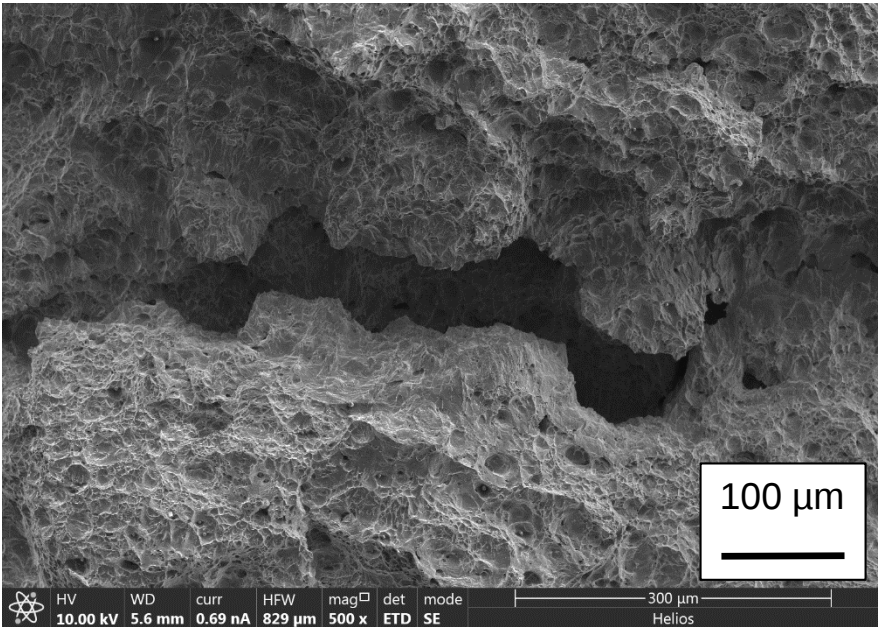


Influence of Argon content on notch toughness – U-notch



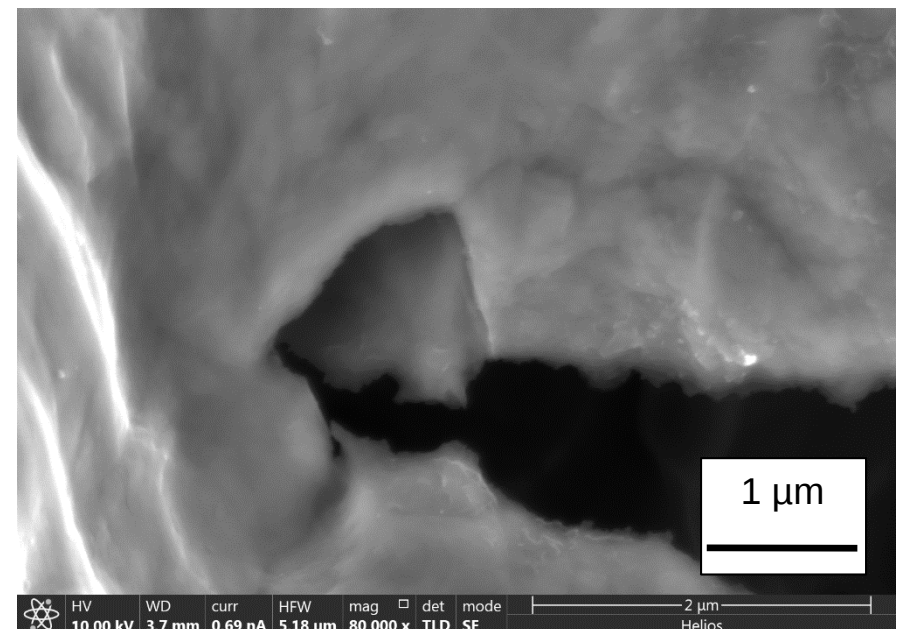
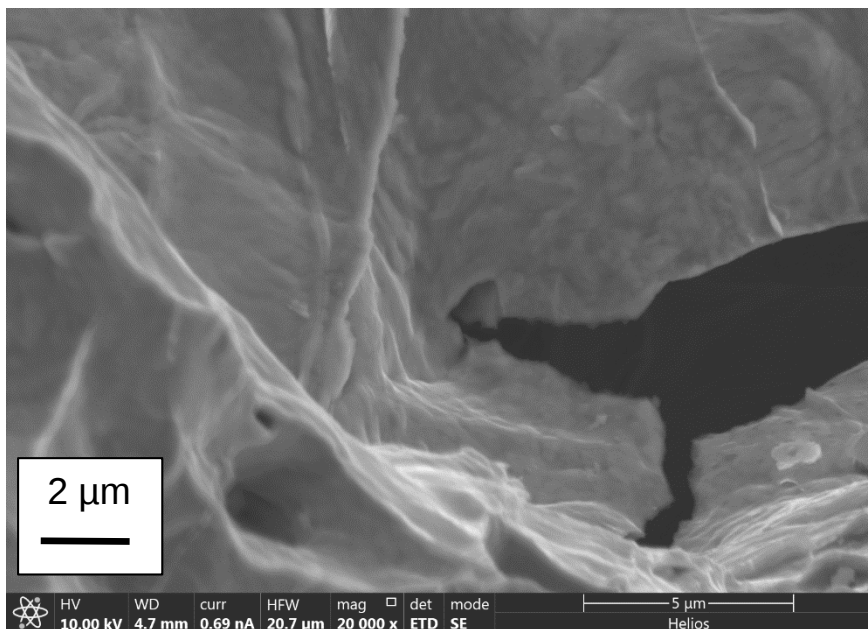
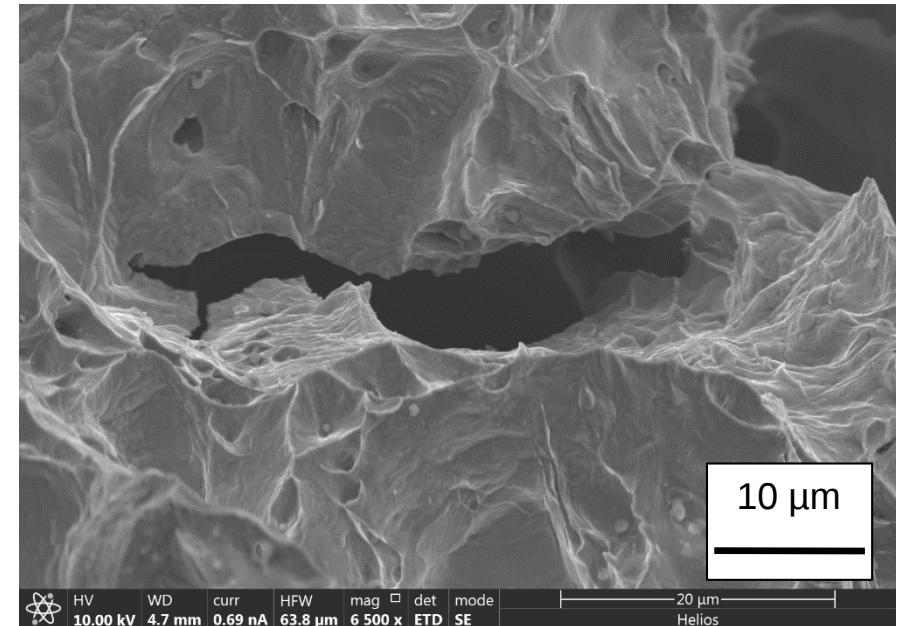
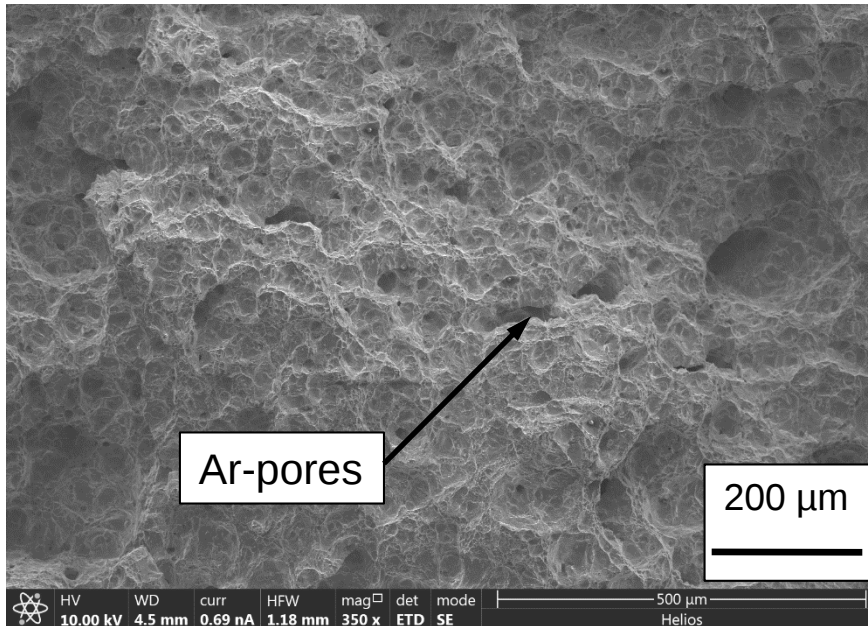
Fracture Surface

PM-HIP - 1 ppm Ar - $T=150\text{ }^{\circ}\text{C}$ - $a_k = 201\text{ J/cm}^2$



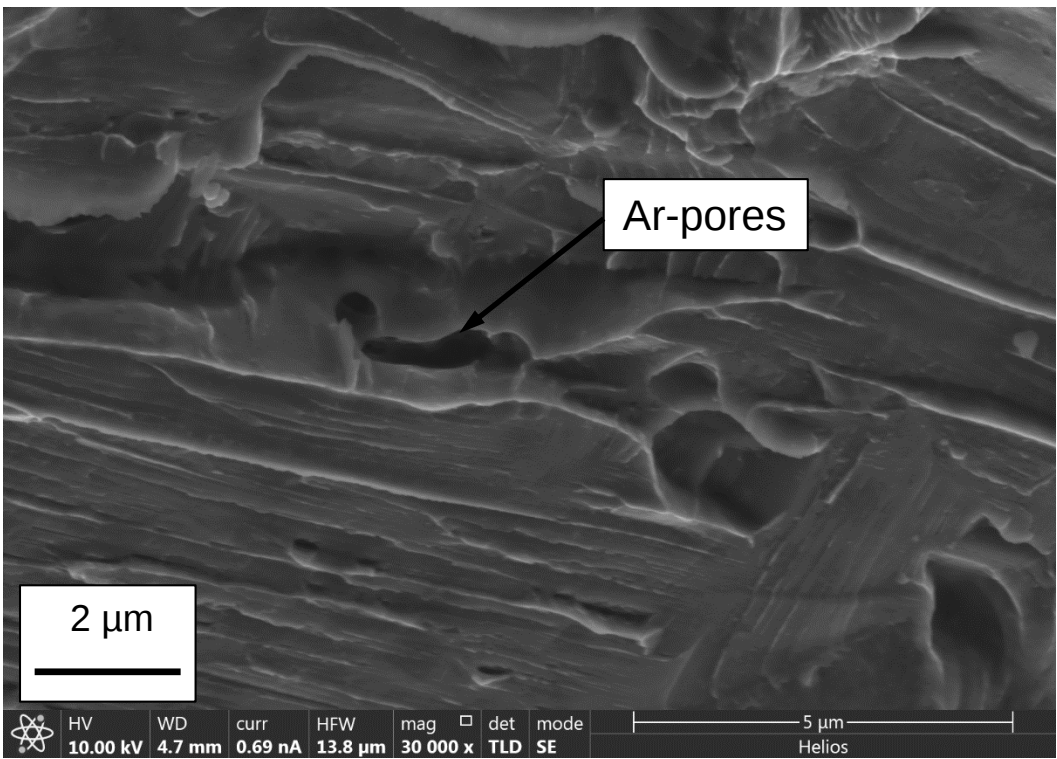
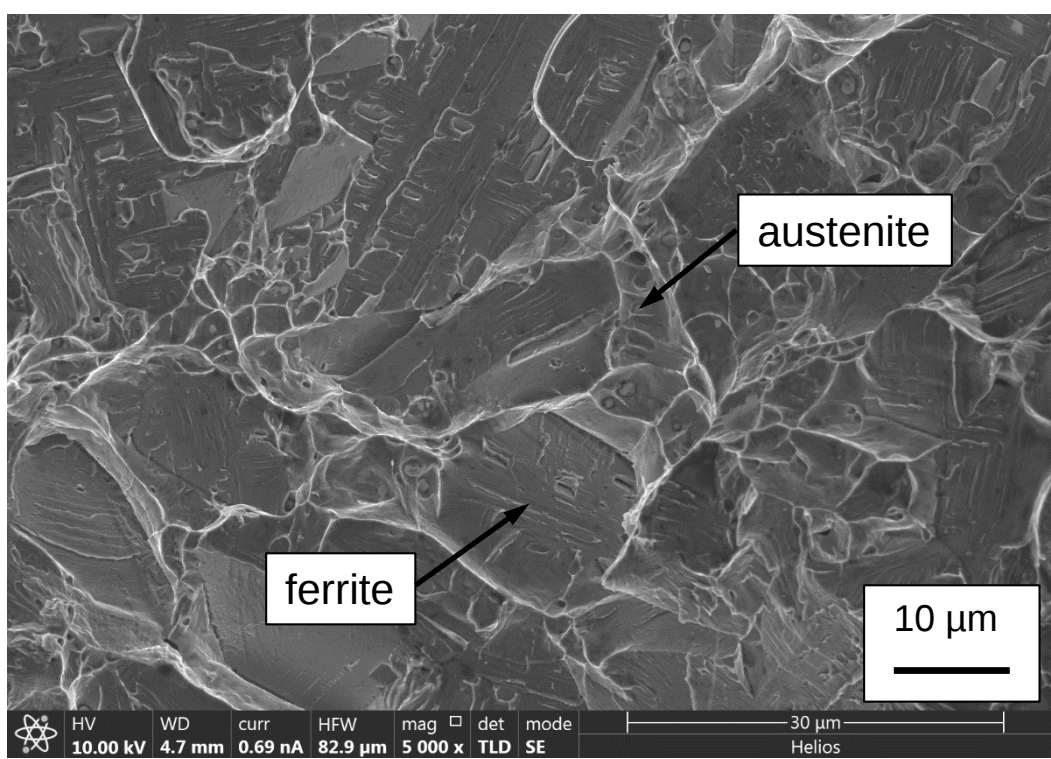
Fracture Surface

PM-HIP – 5.8 ppm Ar - $T=150\text{ }^{\circ}\text{C}$ - $a_k = 91\text{ J/cm}^2$



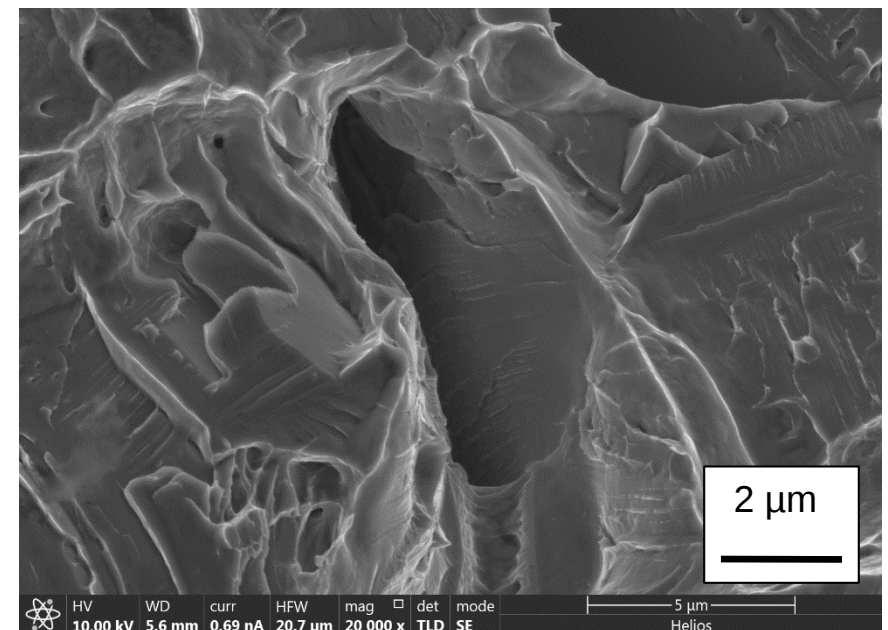
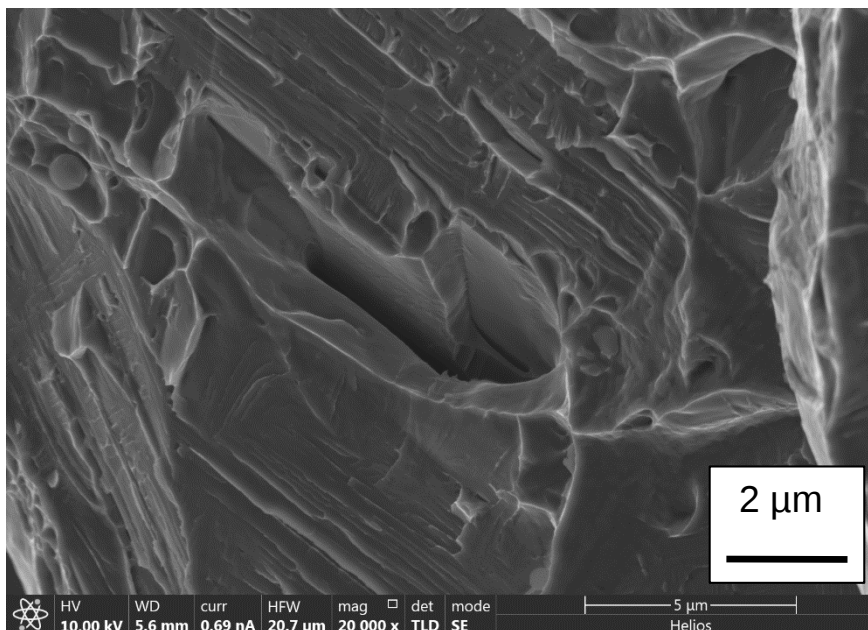
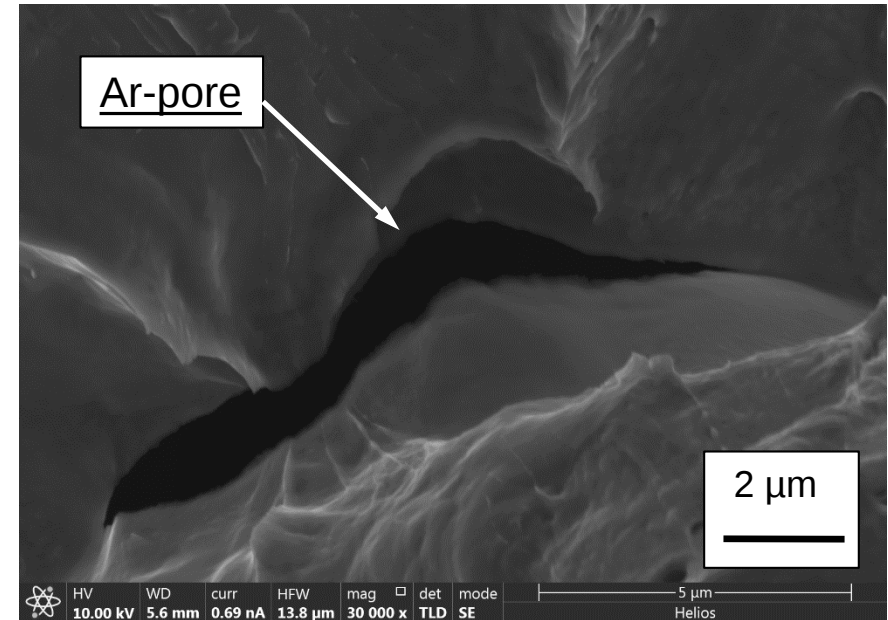
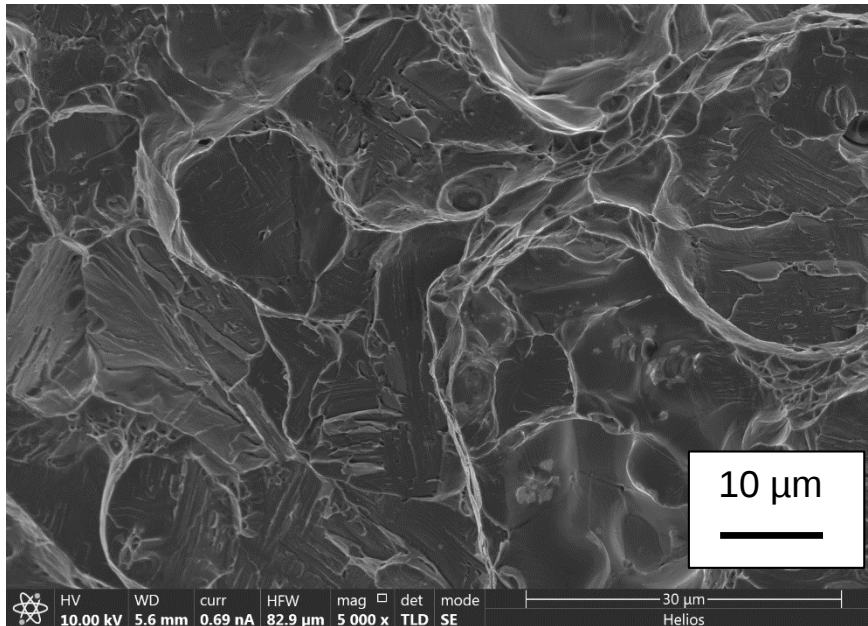
Fracture Surface

PM-HIP - 1 ppm Ar - $T = -185\text{ }^{\circ}\text{C}$ - $a_k = 11\text{ J/cm}^2$



Fracture Surface

PM-HIP – 5.8 ppm Ar - $T = -185\text{ }^{\circ}\text{C}$ - $a_k = 8\text{ J/cm}^2$



- The effects of manufacturing method, heat treatment, notch geometry and Ar-content on the Charpy notch-toughness of AISI 318 duplex steel have been investigated.
- Independent of the testing temperature the toughness of PM-HIP steel is superior to cast material.
- PM-HIP material shows higher toughness compared to forged steel at temperatures lower than -50°C .
- Even a very small amount of σ -phase drastically reduces the toughness.
- A small notch radius leads to an increase of the BDTT and a decrease of the toughness level in the upper shelf.
- Toughness is very sensitive to the Ar content. 90 ppm of Ar lead to brittle fracture even at higher temperatures.

The author would like to thank

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Thank you for your Interest!

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